

EN727005

THERMODYNAMICS FOR CHEMICAL ENGINEERS

อุณหพลศาสตร์สำหรับวิศวกรเคมี

Chapter 6

Thermodynamic Properties of fluids

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6.7 GENERALIZED PROPERTY CORRELATION FOR GASES

$$\frac{H^R}{RT} = -T \int_0^P \left(\frac{\partial Z}{\partial T} \right)_P \frac{dP}{P} \dots (6.46) \quad \frac{S^R}{R} = -T \int_0^P \left(\frac{\partial Z}{\partial T} \right)_P \frac{dP}{P} - \int_0^P (Z-1) \frac{dP}{P} \quad (\text{const } T) \dots (6.48)$$

$$P = P_c P_r \rightarrow dP = P_c dP_r, \quad T = T_c T_r \rightarrow dT = T_c dT_r$$

substitute into Eqs.(6.46) and (6.48):

$$\frac{H^R}{RT_c} = -T_c^2 \int_0^{P_r} \left(\frac{\partial Z}{\partial T_r} \right)_{P_r} \frac{dP_r}{P_r} \dots (6.83)$$

$$\frac{S^R}{R} = T_r \int_0^{P_r} \left(\frac{\partial Z}{\partial T_r} \right)_{P_r} \frac{dP_r}{P_r} - \int_0^{P_r} (Z-1) \frac{dP_r}{P_r} \dots (6.84)$$

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$$Z = Z^0 + \omega Z^1 \rightarrow \left(\frac{\partial Z}{\partial T_r} \right)_{P_r} = \left(\frac{\partial Z^0}{\partial T_r} \right)_{P_r} + \omega \left(\frac{\partial Z^1}{\partial T_r} \right)_{P_r}$$

$$\text{Eq.(6.83): } \frac{H^R}{RT_c} = \left[-T_c^2 \int_0^{P_r} \left(\frac{\partial Z^0}{\partial T_r} \right)_{P_r} \frac{dP_r}{P_r} \right] - \omega \left[T_c^2 \int_0^{P_r} \left(\frac{\partial Z^1}{\partial T_r} \right)_{P_r} \frac{dP_r}{P_r} \right]$$

$$\frac{H^R}{RT_c} = \frac{(H^R)^0}{RT_c} + \omega \frac{(H^R)^1}{RT_c} \dots (6.85)$$

$$\text{Eq.(6.84): } \frac{S^R}{R} = \left[- \int_0^{P_r} \left(T_r \left(\frac{\partial Z^1}{\partial T_r} \right)_{P_r} + Z^0 - 1 \right) \frac{dP_r}{P_r} \right] - \omega \left[\int_0^{P_r} \left(T_r \left(\frac{\partial Z^1}{\partial T_r} \right)_{P_r} + Z^1 \right) \frac{dP_r}{P_r} \right]$$

$$\frac{S^R}{R} = \frac{(S^R)^0}{R} + \omega \frac{(S^R)^1}{R} \dots (6.86)$$

Table E.5 - E.12

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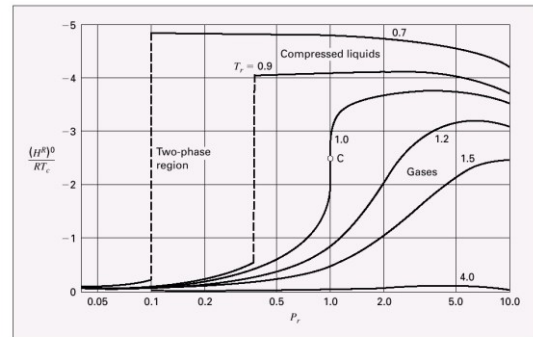


Figure 6.5: The Lee/Kesler correlation for $(H^R)^0 / RT_c$ as a function of T_r and P_r .

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Analytical correlation of the residual properties at low pressure

The generalized second-virial-coefficient correlation forms

$$\hat{B} = \frac{BP_c}{RT_c} = \dots, \quad \frac{d\hat{B}}{dT_r} = \frac{dB^0}{dT_r} + \omega \frac{dB^1}{dT_r}$$

$$\text{Eqs.(6.55) and (6.56): } \frac{H^R}{RT_c} = P_r \left(\hat{B} - T_r \frac{d\hat{B}}{dT_r} \right), \quad \frac{S^R}{R} = -P_r \frac{d\hat{B}}{dT_r}$$

$$\Rightarrow \frac{H^R}{RT_c} = P_r \left[B^0 - T_r \frac{dB^0}{dT_r} + \omega \left(B^1 - T_r \frac{dB^1}{dT_r} \right) \right] \dots (6.87)$$

$$\frac{S^R}{R} = -P_r \left(\frac{dB^0}{dT_r} + \omega \frac{dB^1}{dT_r} \right) \dots (6.88)$$

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$$B^0 = 0.083 - \frac{0.422}{T_r^{1.6}} \dots (3.65)$$

$$B^1 = 0.139 - \frac{0.172}{T_r^{4.2}} \dots (3.66)$$

$$\frac{dB^0}{dT_r} = \frac{0.675}{T_r^{2.6}} \dots (6.89)$$

$$\frac{dB^1}{dT_r} = \frac{0.722}{T_r^{5.2}} \dots (6.90)$$



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H^R and S^R with ideal-gas heat capacities

- For a change from state 1 to 2:

$$H_2 = H_1^R + \int_1^2 C_p^R dT + H_2^R \quad H_1 = H_0^R + \int_0^1 C_p^R dT + H_1^R$$

- The enthalpy change for the process, $\Delta H = H_2 - H_1$

$$\Delta H = \int_{T_1}^{T_2} C_p^R dT + H_2^R - H_1^R \quad \dots (6.91)$$

$$\text{Similarly, } \Delta S = \int_{T_1}^{T_2} C_p^R dT - R \ln \frac{P_2}{P_1} + S_2^R - S_1^R \quad \dots (6.92)$$

- Alternative form

$$\Delta H = \langle C_p^R \rangle_H (T_2 - T_1) + H_2^R - H_1^R \quad \dots (6.93)$$

$$\Delta S = \langle C_p^R \rangle_S \ln \frac{T_2}{T_1} - R \ln \frac{P_2}{P_1} + S_2^R - S_1^R \quad \dots (6.94)$$

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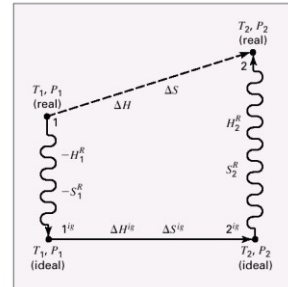


Figure 6.6: Calculational path for property changes ΔH and ΔS .

A three-step calculational path

- Step 1→1^{ig}: A hypothetical process that transforms a real gas into an ideal gas at T_1 and P_1 .

$$H_1^{ig} - H_1 = -H_1^R \quad S_1^{ig} - S_1 = -S_1^R$$

- Step 1^{ig}→2^{ig}: Changes in the ideal-gas state from (T_1, P_1) to (T_2, P_2) .

$$\Delta H^{ig} = H_2^{ig} - H_1^{ig} = \int_{T_1}^{T_2} C_p^{ig} dT \quad \dots (6.95)$$

$$\Delta S^{ig} = S_2^{ig} - S_1^{ig} = \int_{T_1}^{T_2} \frac{C_p^{ig}}{T} dT - R \ln \frac{P_2}{P_1} \quad \dots (6.96)$$

- Step 2^{ig}→2: Another hypothetical process that transform the ideal gas back into a real gas at T_2 and P_2 .

$$H_2 - H_2^{ig} = H_2^R \quad S_2 - S_2^{ig} = S_2^R$$

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Ex. 6.9

Estimate V , U , H and S for 1-butene vapor at 200°C, 70 bar if H and S are set equal to zero for saturated liquid at 0°C.

Assume: $T_c = 420.0$ K, $P_c = 40.43$ bar, $T_n = 266.9$ K, $\omega = 0.191$
 $C_p^{ig}/R = 1.967 + 31.630 \times 10^{-3} T - 9.837 \times 10^{-6} T^2 \quad (T/K)$

Solution

$$T_r = \frac{200 + 273.15}{420.0} = 1.127 \quad P_r = \frac{70}{40.43} = 1.731$$

$$Eq.(3.57) \text{ and Table E.3 and E.4;}$$

$$Z = Z^0 + \omega Z^1 = 0.485 + 0.191(0.142) = 0.512$$

$$V = \frac{ZRT}{P} = \frac{0.512(83.14)(473.15)}{70} = 287.8 \text{ cm}^3 \text{ mol}^{-1}$$

Table E.3: Values of Z^0																Table E.4: Values of Z^2															
$P_r = 1.0000$	1.2000	1.4000	1.6000	1.8000	2.0000	2.2000	2.4000	2.6000	2.8000	3.0000	3.2000	3.4000	3.6000	3.8000	4.0000	$P_r = 1.0000$	1.2000	1.4000	1.6000	1.8000	2.0000	2.2000	2.4000	2.6000	2.8000	3.0000	3.2000	3.4000	3.6000	3.8000	4.0000
0.30	0.2902	0.3479	0.3961	0.4375	0.4750	0.5090	0.5400	0.5680	0.5940	0.6180	0.6400	0.6600	0.6780	0.6940	0.7080	0.30	0.2890	-0.0966	-0.3521	-0.6076	-0.8631	-1.1186	-1.3741	-1.6296	-1.8851	-2.1406	-2.3961	-2.6516	-2.9071	-3.1626	-3.4181
0.35	0.2902	0.3479	0.3961	0.4375	0.4750	0.5090	0.5400	0.5680	0.5940	0.6180	0.6400	0.6600	0.6780	0.6940	0.7080	0.35	0.2890	-0.0966	-0.3521	-0.6076	-0.8631	-1.1186	-1.3741	-1.6296	-1.8851	-2.1406	-2.3961	-2.6516	-2.9071	-3.1626	-3.4181
0.40	0.2902	0.3479	0.3961	0.4375	0.4750	0.5090	0.5400	0.5680	0.5940	0.6180	0.6400	0.6600	0.6780	0.6940	0.7080	0.40	0.2890	-0.0966	-0.3521	-0.6076	-0.8631	-1.1186	-1.3741	-1.6296	-1.8851	-2.1406	-2.3961	-2.6516	-2.9071	-3.1626	-3.4181
0.45	0.2902	0.3479	0.3961	0.4375	0.4750	0.5090	0.5400	0.5680	0.5940	0.6180	0.6400	0.6600	0.6780	0.6940	0.7080	0.45	0.2890	-0.0966	-0.3521	-0.6076	-0.8631	-1.1186	-1.3741	-1.6296	-1.8851	-2.1406	-2.3961	-2.6516	-2.9071	-3.1626	-3.4181
0.50	0.2902	0.3479	0.3961	0.4375	0.4750	0.5090	0.5400	0.5680	0.5940	0.6180	0.6400	0.6600	0.6780	0.6940	0.7080	0.50	0.2890	-0.0966	-0.3521	-0.6076	-0.8631	-1.1186	-1.3741	-1.6296	-1.8851	-2.1406	-2.3961	-2.6516	-2.9071	-3.1626	-3.4181
0.55	0.2902	0.3479	0.3961	0.4375	0.4750	0.5090	0.5400	0.5680	0.5940	0.6180	0.6400	0.6600	0.6780	0.6940	0.7080	0.55	0.2890	-0.0966	-0.3521	-0.6076	-0.8631	-1.1186	-1.3741	-1.6296	-1.8851	-2.1406	-2.3961	-2.6516	-2.9071	-3.1626	-3.4181
0.60	0.2902	0.3479	0.3961	0.4375	0.4750	0.5090	0.5400	0.5680	0.5940	0.6180	0.6400	0.6600	0.6780	0.6940	0.7080	0.60	0.2890	-0.0966	-0.3521	-0.6076	-0.8631	-1.1186	-1.3741	-1.6296	-1.8851	-2.1406	-2.3961	-2.6516	-2.9071	-3.1626	-3.4181
0.65	0.2902	0.3479	0.3961	0.4375	0.4750	0.5090	0.5400	0.5680	0.5940	0.6180	0.6400	0.6600	0.6780	0.6940	0.7080	0.65	0.2890	-0.0966	-0.3521	-0.6076	-0.8631	-1.1186	-1.3741	-1.6296	-1.8851	-2.1406	-2.3961	-2.6516	-2.9071	-3.1626	-3.4181
0.70	0.2902	0.3479	0.3961	0.4375	0.4750	0.5090	0.5400	0.5680	0.5940	0.6180	0.6400	0.6600	0.6780	0.6940	0.7080	0.70	0.2890	-0.0966	-0.3521	-0.6076	-0.8631	-1.1186	-1.3741	-1.6296	-1.8851	-2.1406	-2.3961	-2.6516	-2.9071	-3.1626	-3.4181
0.75	0.2902	0.3479	0.3961	0.4375	0.4750	0.5090	0.5400	0.5680	0.5940	0.6180	0.6400	0.6600	0.6780	0.6940	0.7080	0.75	0.2890	-0.0966	-0.3521	-0.6076	-0.8631	-1.1186	-1.3741	-1.6296	-1.8851	-2.1406	-2.3961	-2.6516	-2.9071	-3.1626	-3.4181
0.80	0.2902	0.3479	0.3961	0.4375	0.4750	0.5090	0.5400	0.5680	0.5940	0.6180	0.6400	0.6600	0.6780	0.6940	0.7080	0.80	0.2890	-0.0966	-0.3521	-0.6076	-0.8631	-1.1186	-1.3741	-1.6296	-1.8851	-2.1406	-2.3961	-2.6516	-2.9071	-3.1626	-3.4181
0.85	0.2902	0.3479	0.3961	0.4375	0.4750	0.5090	0.5400	0.5680	0.5940	0.6180	0.6400	0.6600	0.6780	0.6940	0.7080	0.85	0.2890	-0.0966	-0.3521	-0.6076	-0.8631	-1.1186	-1.3741	-1.6296	-1.8851	-2.1406	-2.3961	-2.6516	-2.9071	-3.1626	-3.4181
0.90	0.2902	0.3479	0.3961	0.4375	0.4750	0.5090	0.5400	0.5680	0.5940	0.6180	0.6400	0.6600	0.6780	0.6940	0.7080	0.90	0.2890	-0.0966	-0.3521	-0.6076	-0.8631	-1.1186	-1.3741	-1.6296	-1.8851	-2.1406	-2.3961	-2.6516	-2.9071	-3.1626	-3.4181
0.95	0.2902	0.3479	0.3961	0.4375	0.4750	0.5090	0.5400	0.5680	0.5940	0.6180	0.6400	0.6600	0.6780	0.6940	0.7080	0.95	0.2890	-0.0966	-0.3521	-0.6076	-0.8631	-1.1186	-1.3741	-1.6296	-1.8851	-2.1406	-2.3961	-2.6516	-2.9071	-3.1626	-3.4181
1.00	0.2902	0.3479	0.3961	0.4375	0.4750	0.5090	0.5400	0.5680	0.5940	0.6180	0.6400	0.6600	0.6780	0.6940	0.7080	1.00	0.2890	-0.0966	-0.3521	-0.6076	-0.8631	-1.1186	-1.3741	-1.6296	-1.8851	-2.1406	-2.3961	-2.6516	-2.9071	-3.1626	-3.4181
1.05	0.2902	0.3479	0.3961	0.4375	0.4750	0.5090	0.5400	0.5680	0.5940	0.6180	0.6400	0.6600	0.6780	0.6940	0.7080	1.05	0.2890	-0.0966	-0.3521	-0.6076	-0.8631	-1.1186	-1.3741	-1.6296	-1.8851	-2.1406	-2.3961	-2.6516	-2.9071	-3.1626	-3.4181
1.10	0.2902	0.3479	0.3961	0.4375	0.4750	0.5090	0.5400	0.5680	0.5940	0.6180	0.6400	0.6600	0.6780	0.6940	0.7080	1.10	0.2890	-0.0966	-0.3521	-0.6076	-0.8631	-1.1186	-1.3741	-1.6296	-1.8851	-2.1406	-2.3961	-2.6516	-2.9071	-3.1626	-3.4181
1.15	0.2902	0.3479	0.3961	0.4375	0.4750	0.5090	0.5400	0.5680	0.5940	0.6180	0.6400	0.6600	0.6780	0.6940	0.7080	1.15	0.2890	-0.0966	-0.3521	-0.6076	-0.8631	-1.1186	-1.3741	-1.6296	-1.8851	-2.1406	-2.3961	-2.6516	-2.9071	-3.1626	-3.4181
1.20	0.2902	0.3479	0.3961	0.4375	0.4750	0.5090	0.5400	0.5680	0.5940	0.6180	0.6400	0.6600	0.6780	0.6940	0.7080	1.20	0.2890	-0.0966	-0.3521	-0.6076	-0.8631	-1.1186	-1.3741	-1.6296	-1.8851	-2.1406	-2.3961	-2.6516	-2.9071	-3.1626	-3.4181
1.25	0.2902	0.3479	0.3961	0.4375	0.4750	0.5090	0.5400	0.5680	0.5940	0.6180	0.6400	0.6600	0.6780	0.6940	0.7080	1.25	0.2890	-0.0966	-0.3521	-0.6076	-0.8631	-1.1186	-1.3741	-1.6296	-1.8851	-2.1406	-2.3961	-2.6516	-2.9071	-3.1626	-3.4181
1.30	0.2902	0.3479	0.3961	0.4375	0.4750	0.5090	0.5400	0.5680	0.5940	0.6180	0.6400	0.6600	0.6780	0.6940	0.7080	1.30	0.2890	-0.0966	-0.3521	-0.6076	-0.8631	-1.1186	-1.3741	-1.6296	-1.8851	-2.1406	-2.3961	-2.6516	-2.9071	-3.1626	-3.4181
1.35	0.2902	0.3479	0.3961	0.4375	0.4750	0.5090	0.5400	0.5680	0.5940	0.6180	0.6400	0.6600	0.6780	0.6940	0.7080	1.35	0.2890	-0.0966	-0.3521	-0.6076	-0.8631	-1.1186	-1.3741	-1.6296	-1.8851	-2.1406	-2.3961	-2.6516	-2.9071	-3.1626	-3.4181
1.40	0.2902	0.3479	0.3961	0.4375	0.4750	0.5090	0.5400	0.5680	0.5940	0.6180	0.6400	0.6600	0.6780	0.6940	0.7080	1.40	0.2890	-0.0966	-0.3521	-0.6076	-0.8631	-1.1186	-1.3741	-1.6296	-1.8851	-2.1406	-2.3961	-2.6516	-2.9071	-3.1626	-3.4181
1.45	0.2902	0.3479	0.3961	0.4375	0.4750	0.5090	0.5400	0.5680	0.5940	0.6180	0.6400	0.6600	0.6780	0.6940	0.7080	1.45	0.2890	-0.0966	-0.3521	-0.6076	-0.8631	-1.1186	-1.3741	-1.6296	-1.8851	-2.1406	-2.3961	-2.6516	-2.9071	-3.1626	-3.4181
1.50	0.2902	0.3479	0.3961	0.4375	0.4750	0.5090	0.5400	0.5680	0.5940	0.6180	0.6400	0.6600	0.6780	0.6940	0.7080	1.50	0.2890	-0.0966	-0.3521	-0.6076	-0.8631	-1.1186	-1.3741	-1.6296	-1.8851	-2.1406	-2.3961	-2.6516	-2.9071	-3.1626	-3.4181
1.55	0.2902	0.3479	0.3961	0.4375	0.4750	0.5090	0.5400	0.5680	0.5940	0.6180	0.6400	0.6600	0.6780	0.6940	0.7080	1.55	0.2890	-0.0966	-0.3521	-0.6076	-0.8631	-1.1186	-1.3741	-1.6296	-1.8851	-2.1406	-2.3961	-2.6516	-2.9071	-3.1626	-3.4181
1.60	0.2902	0.3479	0.3961	0.4375	0.4750	0.5090	0.5400	0.5680	0.5940	0.6180	0.6400	0.6600	0.6780	0.6940	0.7080	1.60	0.2890	-0.0966	-0.3521	-0.6076	-0.8631	-1.1186	-1.3741	-1.6296	-1.8851	-2.1406	-2.3961	-2.6516	-2.9071	-3.1626	-3.4181
1.65	0.2902	0.3479	0.3961	0.4375	0.4750	0.5090	0.5400	0.5680	0.5940	0.6180	0.6400	0.6600	0.6780	0.6940	0.7080	1.65	0.2890	-0.0966	-0.3521	-0.6076	-0.8631	-1.1186	-1.3741	-1.6296	-1.8851	-2.1406	-2.3961	-2.6516	-2.9071	-3.1626	-3.4181
1.70	0.2902	0.3479	0.3961	0.4375	0.4750	0.5090	0.5400	0.5680	0.5940	0.6180	0.6400	0.6600	0.6780	0.6940	0.7080	1.70	0.2890	-0.0966	-0.3521	-0.6076	-0.8631	-1.1186	-1.3741	-1.6296	-1.8851	-2.1406	-2.3961	-2.6516	-2.9071	-3.1626	-3.4181
1.75	0.2902	0.3479	0.3961	0.4375	0.4750	0.5090	0.5400	0.5680	0.5940	0.6180	0.6400	0.6600	0.6780	0.6940	0.7080	1.75	0.2890	-0.0966	-0.3521	-0.6076	-0.8631	-1.1186	-1.3741	-1.6296	-1.8851	-2.1406	-2.3961	-2.6516	-2.9071	-3.1626	-3.4181
1.80	0.2902	0.3479	0.3961	0.4375	0.4750	0.5090	0.5400	0.5680	0.5940	0.6180	0.6400	0.6600	0.6780	0.6940	0.7080	1.80	0.2890	-0.0966	-0.3521	-0.6076	-0.8631	-1.1186	-1.3741	-1.6296	-1.8851	-2.1406	-2.3961	-2.6516	-2.9071	-3.1626	-3.4181
1.85	0.2902	0.3479	0.3961	0.4375	0.4750	0.5090	0.5400	0.5680	0.5940	0.6180	0.6400	0.6600	0.6780	0.6940	0.7080	1.85	0.2890	-0.0966	-0.3521	-0.6076	-0.8631	-1.1186	-1.3741	-1.6296	-1.8851	-2.1406	-2.3961	-2.6516	-2.9071	-3.1626	-3.4181
1.90	0.2902	0.3479	0.3961	0.4375	0.4750	0.5090	0.5400	0.5680	0.5940	0.6180	0.6400	0.6600	0.6780	0.6940	0.7080	1.90	0.2890	-0.0966	-0.3521	-0.6076	-0.8631	-1.1186	-1.3741	-1.6296	-1.8851	-2.1406	-2.3961	-2.6516	-2.9071	-3.1626	-3.4181
1.95	0.2902	0.3479	0.3961	0.4375	0.4750	0.5090	0.5400	0.5680	0.5940	0.6180	0.6400	0.6600	0.6780	0.6940	0.7080	1.95	0.2890	-0.0966	-0.3521	-0.6076	-0.8631	-1.1186	-1.3741	-1.6296	-1.8851	-2.1406	-2.3961	-2.6516	-2.9071	-3.1626	-3.418

- Step (a): Vaporization of saturated liquid 1-butane at 0°C

$$\ln P^{\text{sat}} = A - \frac{B}{T} \quad \dots (6.75)$$

- The vapor pressure curve contains both
the normal boiling point; $\ln 1.0133 = A - \frac{B}{266.9}$
the critical point; $\ln 40.43 = A - \frac{B}{420.0}$

$$\text{Whence, } A = 10.126 \quad B = 2,699.11$$

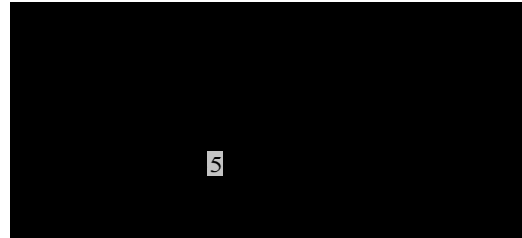
$$\Delta H = T \Delta V \frac{dP^{\text{sat}}}{dT} \quad (4.11) \quad \frac{\Delta H_2}{\Delta H_1} = \left(\frac{1 - T_{r2}}{1 - T_{r1}} \right)^{0.38} \quad (4.13)$$

- The latent heat of vaporization, where $T_{r1} = 266.9/420 = 0.635$:

$$\frac{\Delta H_n^{\text{lv}}}{RT_n} = \frac{1.092(\ln P_c - 1.013)}{0.930 - T_{r1}} = \frac{1.092(\ln 40.43 - 1.013)}{0.930 - 0.636} = 9.979$$

$$\Delta H_n^{\text{lv}} = (9.979)(8.314)(266.9) = 22,137 \text{ J mol}^{-1} \quad 68$$

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- Step (b): Transformation of saturated vapor into an ideal gas at (T_1, P_1) .

$$\frac{H^R}{RT_r} = P_r \left[B^0 - T_r \frac{dB^0}{dT_r} + \omega \left(B^1 - T_r \frac{dB^1}{dT_r} \right) \right] \quad (6.87) \quad B^0 = 0.083 - \frac{0.422}{T_r^{1.6}} \quad \dots (3.65)$$

$$B^1 = 0.139 - \frac{0.172}{T_r^{4.2}} \quad \dots (3.66)$$

$$\frac{S^R}{R} = -P_r \left(\frac{dB^0}{dT_r} + \omega \frac{dB^1}{dT_r} \right) \quad \dots (6.88) \quad \frac{dB^0}{dT_r} = \frac{0.675}{T_r^{2.6}} \quad \dots (6.89)$$

$$\frac{dB^1}{dT_r} = \frac{0.722}{T_r^{5.2}} \quad \dots (6.90)$$

- $T_r = 0.650$ and $P_r = 1.2771/40.43 = 0.0316$

$$\text{So, } H_1^R = (-0.0985)(8.314)(420) = \text{[redacted]}$$

$$S_1^R = (-0.1063)(8.314) = -0.88 \text{ J mol}^{-1} \text{ K}^{-1}$$

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- Step (c): Changes in the ideal gas state

$$\text{Eq. (6.95): } \Delta H^g = H_2^g - H_1^g = \int_{T_1}^{T_2} C_p^g dT = \langle C_p^g \rangle_n (T_2 - T_1)$$

$$\text{Eq. (6.96): } \Delta S^g = S_2^g - S_1^g = \int_{T_1}^{T_2} C_p^g \frac{dT}{T} - R \ln \frac{P_2}{P_1} = \langle C_p^g \rangle_n \ln \frac{T_2}{T_1} - R \ln \frac{P_2}{P_1}$$

- $T_{\text{am}} = 373.15 \text{ K}$, $T_{\text{im}} = 364.04 \text{ K}$,
 $A = 1.967$, $B = 31.630 \times 10^{-3}$, $C = -9.837 \times 10^{-6}$

$$\Delta H^g = \text{[redacted]}$$

$$\Delta S^g = 22.18 \text{ J mol}^{-1} \text{ K}^{-1}$$

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- Step (d): Transformation from the ideal gas to real gas state at T_2 and P_2 .

$$T_r = 1.127 \quad P_r = 1.731 \quad \frac{H^R}{RT_r} = \left[\frac{B^0}{T_r} - \frac{dB^0}{dT_r} + \omega \left(\frac{B^1}{T_r} - \frac{dB^1}{dT_r} \right) \right] \quad (6.85)$$

- At the higher P ; Eqs. (6.85) and (6.86) with interpolated values from Table E.7, E.8, E.11 and E.12.

$$\frac{H^R}{RT_c} = -2.294 + (0.191)(-0.713) = -2.430$$

$$\frac{S^R}{R} = -1.566 + (0.191)(-0.726) = -1.705$$

$$\Rightarrow H_2^R = (-2.430)(8.314)(420.0) = \text{[redacted]}$$

$$S_2^R = (-1.705)(8.314) = -14.18 \text{ J mol}^{-1} \text{ K}^{-1}$$



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Extension to Gas Mixtures

$$\omega = \sum_i y_i \omega_i \quad \dots (6.97) \quad T_{pc} = \sum_i y_i T_{ci} \quad \dots (6.98) \quad P_{pc} = \sum_i y_i P_{ci} \quad \dots (6.99)$$

$$T_{pr} = \frac{T}{T_{pc}} \quad \dots (6.100) \quad P_{pr} = \frac{P}{P_{pc}} \quad \dots (6.101)$$

These replace T_r and P_r for reading entries from the table of App. E, and lead to values of Z by Eq.(3.57), and H^R/RT_{pc} by Eq.(6.85), and S^R/R by Eq.(6.86).

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Ex. 6.10

Estimate V , H^R , and S^R for an equimolar mixture of carbon dioxide(1) and propane(2) at 450 K and 140 bar by the Lee/Kesler correlations.

Solution

From Table B.1,

$$\omega = y_1 \omega_1 + y_2 \omega_2 = (0.5)(\overset{\text{CO}_2}{0.224}) + (0.5)(\overset{\text{propane}}{0.152}) = 0.188$$

$$T_{pc} = y_1 T_{c1} + y_2 T_{c2} = (0.5)(304.2) + (0.5)(369.8) = 337.0 \text{ K}$$

$$P_{pc} = y_1 P_{c1} + y_2 P_{c2} = (0.5)(73.83) + (0.5)(42.48) = 58.15 \text{ bar}$$

$$\text{Whence, } T_{pr} = \frac{450}{337.0} = 1.335 \quad P_{pr} = \frac{140}{58.15} = 2.41$$

Table B.I. Characterization properties of Pure Species							Table B.II. (Continued)								
Molar mass	m	V_m	E_{HOMO}	E_{LUMO}	E_g	V_{HOMO}	Molar mass	m	V_m	E_{HOMO}	E_{LUMO}	E_g	V_{HOMO}		
Methane	16.043	0.022	198.66	65.99	0.286	98.6	11.8	Methanol	32.062	0.044	57.62	32.09	0.224	118	337.9
Ethane	30.070	0.044	198.66	65.99	0.286	98.6	11.8	Ethanol	46.069	0.066	57.62	32.09	0.224	118	337.9
Propane	44.097	0.067	198.66	65.99	0.286	98.6	11.8	1-Propanol	60.096	0.082	58.08	31.78	0.234	119	338.0
Butane	58.124	0.089	198.66	65.99	0.286	98.6	11.8	2-Propanol	60.096	0.082	58.08	31.78	0.234	119	338.0
n-Pentane	72.150	0.102	198.66	65.99	0.286	98.6	11.8	1-Pentanol	102.177	0.179	57.94	31.50	0.263	121	400.6
n-Hexane	86.177	0.125	198.66	65.99	0.286	98.6	11.8	2-Pentanol	102.177	0.179	57.94	31.50	0.263	121	400.6
n-Heptane	100.204	0.148	198.66	65.99	0.286	98.6	11.8	3-Pentanol	102.177	0.179	57.94	31.50	0.263	121	400.6
n-Octane	114.231	0.170	198.66	65.99	0.286	98.6	11.8	Phenol	94.113	0.044	69.05	31.81	0.243	120	405.0
n-Nonane	128.258	0.194	198.66	65.99	0.286	98.6	11.8	Phenyl glycidyl ether	150.171	0.309	57.94	31.50	0.263	121	400.6
n-Decane	142.285	0.217	198.66	65.99	0.286	98.6	11.8	Acetic acid	60.052	0.057	57.96	32.11	1.797	161	371.7
n-Undecane	156.312	0.239	198.66	65.99	0.286	98.6	11.8	Formic acid	46.027	0.039	57.96	32.11	1.797	161	371.7
n-Dodecane	170.339	0.262	198.66	65.99	0.286	98.6	11.8	Benzoic acid	122.120	0.030	73.19	43.49	0.246	134	522.4
n-Tridecane	184.366	0.284	198.66	65.99	0.286	98.6	11.8	Hexanoic acid	146.198	0.091	69.05	31.81	0.243	120	405.0
Cyclopentane	70.134	0.196	118.1	49.02	0.273	288	324.4	Methyl laurate	310.071	0.811	74.04	32.31	1.34	268	848.8
Cyclohexane	98.150	0.270	118.1	49.02	0.273	288	324.4	Octyl laurate	338.534	0.872	74.04	32.31	1.34	268	848.8
Methylcyclopentane	84.161	0.210	132.58	37.85	0.272	319	345.0	Acetone	58.080	0.039	57.96	32.11	1.797	161	371.7
Methylcyclohexane	98.150	0.270	132.58	37.85	0.272	319	345.0	Acetophenone	134.125	0.039	69.05	31.81	0.243	120	405.0
Ethylcyclopentane	102.177	0.282	132.58	37.85	0.272	319	345.0	Phenylacetone	134.125	0.039	69.05	31.81	0.243	120	405.0
Ethylcyclohexane	116.204	0.307	132.58	37.85	0.272	319	345.0	Dichloromethane	84.932	0.099	58.08	31.69	0.265	125	312.9
1,4-Dioxane	98.150	0.270	132.58	37.85	0.272	319	345.0	Ethyl dichloromethane	133.041	0.099	58.08	31.69	0.265	125	312.9
1,4-Dioxane	98.150	0.270	132.58	37.85	0.272	319	345.0	Ethyl trichloromethane	162.030	0.099	58.08	31.69	0.265	125	312.9
2-Methoxy-1,4-dioxane	126.176	0.318	132.58	37.85	0.272	319	345.0	Tetrahydrofuran	72.046	0.044	54.14	30.79	0.275	109	263.4
2-Ethoxy-1,4-dioxane	140.203	0.341	132.58	37.85	0.272	319	345.0	Thiophene	108.147	0.044	54.14	30			
2,5-Dimethoxy-1,4-dioxane	154.231	0.363	132.58	37.85	0.272	319	345.0	Thiophene	108.147	0.044	54.14	30			
2-Ethoxy-2,5-dimethoxy-1,4-dioxane	186.207	0.427	132.58	37.85	0.272	319	345.0	Thiophene	108.147	0.044	54.14	30			
2,5-Dimethoxy-2-ethyl-1,4-dioxane	200.234	0.450	132.58	37.85	0.272	319	345.0	Thiophene	108.147	0.044	54.14	30			
2-Ethoxy-2,5-dimethoxy-2-ethyl-1,4-dioxane	232.208	0.514	132.58	37.85	0.272	319	345.0	Thiophene	108.147	0.044	54.14	30			
2-Ethoxy-2,5-dimethoxy-2-ethyl-1,4-dioxane	232.208	0.514	132.58	37.85	0.272	319	345.0	Thiophene	108.147	0.044	54.14	30			
2-Ethoxy-2,5-dimethoxy-2-ethyl-1,4-dioxane	232.208	0.514	132.58	37.85	0.272	319	345.0	Thiophene	108.147	0.044	54.14	30			
2-Ethoxy-2,5-dimethoxy-2-ethyl-1,4-dioxane	232.208	0.514	132.58	37.85	0.272	319	345.0	Thiophene	108.147	0.044	54.14	30			
2-Ethoxy-2,5-dimethoxy-2-ethyl-1,4-dioxane	232.208	0.514	132.58	37.85	0.272	319	345.0	Thiophene	108.147	0.044	54.14	30			
2-Ethoxy-2,5-dimethoxy-2-ethyl-1,4-dioxane	232.208	0.514	132.58	37.85	0.272	319	345.0	Thiophene	108.147	0.044	54.14	30			
2-Ethoxy-2,5-dimethoxy-2-ethyl-1,4-dioxane	232.208	0.514	132.58	37.85	0.272	319	345.0	Thiophene	108.147	0.044	54.14	30			
2-Ethoxy-2,5-dimethoxy-2-ethyl-1,4-dioxane	232.208	0.514	132.58	37.85	0.272	319	345.0	Thiophene	108.147	0.044	54.14	30			
2-Ethoxy-2,5-dimethoxy-2-ethyl-1,4-dioxane	232.208	0.514	132.58	37.85	0.272	319	345.0	Thiophene	108.147	0.044	54.14	30			
2-Ethoxy-2,5-dimethoxy-2-ethyl-1,4-dioxane	232.208	0.514	132.58	37.85	0.272	319	345.0	Thiophene	108.147	0.044	54.14	30			
2-Ethoxy-2,5-dimethoxy-2-ethyl-1,4-dioxane	232.208	0.514	132.58	37.85	0.272	319	345.0	Thiophene	108.147	0.044	54.14	30			
2-Ethoxy-2,5-dimethoxy-2-ethyl-1,4-dioxane	232.208	0.514	132.58	37.85	0.272	319	345.0	Thiophene	108.147	0.044	54.14	30			
2-Ethoxy-2,5-dimethoxy-2-ethyl-1,4-dioxane	232.208	0.514	132.58	37.85	0.272	319	345.0	Thiophene	108.147	0.044	54.14	30			
2-Ethoxy-2,5-dimethoxy-2-ethyl-1,4-dioxane	232.208	0.514	132.58	37.85	0.272	319	345.0	Thiophene	108.147	0.044	54.14	30			
2-Ethoxy-2,5-dimethoxy-2-ethyl-1,4-dioxane	232.208	0.514	132.58	37.85	0.272	319	345.0	Thiophene	108.147	0.044	54.14	30			
2-Ethoxy-2,5-dimethoxy-2-ethyl-1,4-dioxane	232.208	0.514	132.58	37.85	0.272	319	345.0	Thiophene	108.147	0.044	54.14	30			
2-Ethoxy-2,5-dimethoxy-2-ethyl-1,4-dioxane	232.208	0.514	132.58	37.85	0.272	319	345.0	Thiophene	108.147	0.044	54.14	30			
2-Ethoxy-2,5-dimethoxy-2-ethyl-1,4-dioxane	232.208	0.514	132.58	37.85	0.272	319	345.0	Thiophene	108.147	0.044	54.14	30			
2-Ethoxy-2,5-dimethoxy-2-ethyl-1,4-dioxane	232.208	0.514	132.58	37.85	0.272	319	345.0	Thiophene	108.147	0.044	54.14	30			
2-Ethoxy-2,5-dimethoxy-2-ethyl-1,4-dioxane	232.208	0.514	132.58	37.85	0.272	319	345.0	Thiophene	108.147	0.044	54.14	30			
2-Ethoxy-2,5-dimethoxy-2-ethyl-1,4-dioxane	232.208	0.514	132.58	37.85	0.272	319	345.0	Thiophene	108.147	0.044	54.14	30			
2-Ethoxy-2,5-dimethoxy-2-ethyl-1,4-dioxane	232.208	0.514	132.58	37.85	0.272	319	345.0	Thiophene	108.147	0.044	54.14	30			
2-Ethoxy-2,5-dimethoxy-2-ethyl-1,4-dioxane	232.208	0.514	132.58	37.85	0.272	319	345.0	Thiophene	108.147	0.044	54.14	30			
2-Ethoxy-2,5-dimethoxy-2-ethyl-1,4-dioxane	232.208	0.514	132.58	37.85	0.272	319	345.0	Thiophene	108.147	0.044	54.14	30			
2-Ethoxy-2,5-dimethoxy-2-ethyl-1,4-dioxane	232.208	0.514	132.58	37.85	0.272	319	345.0	Thiophene	108.147	0.044	54.14	30			
2-Ethoxy-2,5-dimethoxy-2-ethyl-1,4-dioxane	232.208	0.514	132.58	37.85	0.272	319	345.0	Thiophene	108.147	0.044	54.14	30			
2-Ethoxy-2,5-dimethoxy-2-ethyl-1,4-dioxane	232.208	0.514	132.58	37.85	0.272	319	345.0	Thiophene	108.147	0.044	54.14	30			
2-Ethoxy-2,5-dimethoxy-2-ethyl-1,4-dioxane	232.208	0.514	132.58	37.85	0.272	319	345.0	Thiophene	108.147	0.044	54.14	30			
2-Ethoxy-2,5-dimethoxy-2-ethyl-1,4-dioxane	232.208	0.514	132.58	37.85	0.272	319	345.0	Thiophene	108.147	0.044	54.14	30			
2-Ethoxy-2,5-dimethoxy-2-ethyl-1,4-dioxane	232.208	0.514	132.58	37.85	0.272	319	345.0	Thiophene	108.147	0.044	54.14	30			
2-Ethoxy-2,5-dimethoxy-2-ethyl-1,4-dioxane	232.208	0.514	132.58	37.85	0.272	319	345.0	Thiophene	108.147	0.044	54.14	30			
2-Ethoxy-2,5-dimethoxy-2-ethyl-1,4-dioxane	232.208	0.514	132.58	37.85	0.272	319	345.0	Thiophene	108.147	0.044	54.14	30			
2-Ethoxy-2,5-dimethoxy-2-ethyl-1,4-d															

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[†] Pseudoparameters for $\eta_{O_2} = 0.79$ and $\eta_{O_1} = 0.21$. See Eqs. (6.97)–(6.99).

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From Table E.3 and E.4;

$$Z = Z^0 + \omega Z^1 = 0.697 + (0.188)(0.205) = 0.736$$

$$\Rightarrow V = \frac{ZRT}{P} = \frac{(0.736)(83.14)(450)}{140} = 196.7 \text{ cm}^3 \text{ mol}^{-1}$$

From Table E.7 and E.8; with Eq.(6.85):

$$\left(\frac{H^R}{RT_{pc}}\right)^0 = -1.730 \quad \left(\frac{H^R}{RT_{pc}}\right)^1 = -0.169$$

$$\frac{H^R}{RT_{pc}} = -1.730 + (0.188)(-0.169) = -1.762$$

$$H^R = (8.314)(337)(-1.762) = -4,937 \text{ Jmol}^{-1}$$

From Table E.11 and E.12; with Eq.(6.86):

$$\frac{S^R}{R} = -0.967 + (0.188)(-0.330) = -1.029$$

$$S^R = (8.314)(-1.029) = -8.56 J mol^{-1} K^{-1}$$

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End of Part 3

