

ภาควิชาวิศวกรรมเครื่องกล

คณะวิศวกรรมศาสตร์ มหาวิทยาลัยขอนแก่น

ข้อสอบปลายภาค ประจำภาคปลาย ปีการศึกษา 2552

วิชา 185 232 Thermodynamics II

วันที่ 25 กุมภาพันธ์ 2553

เวลา 13.00-16.00 น.

ผู้ออกและตรวจข้อสอบ: รศ.ดร.สมหมาย ปรีเปรม

คำสั่ง

1. ให้เขียน ชื่อ-สกุล กลุ่ม ห้องสอบ และ ที่นั่งสอบ ลงในกระดาษข้อสอบทุกแผ่น
2. ข้อสอบทั้งหมดมี 6 ข้อ จำนวน 7 แผ่นรวมทั้งแผ่นนี้ ให้ทำทุกข้อ
3. มีตาราง Thermodynamics แจกให้ ห้ามขีดเขียนในตารางโดยเด็ดขาด
4. อนุญาตให้ใช้เครื่องคำนวณที่ไม่มีการบันทึกข้อมูลของรายวิชานี้ไว้
5. ห้ามนำเอกสารใดๆออกจากห้องสอบ
6. ให้ทำข้อสอบในแผ่นข้อสอบของข้อนั้นๆเท่านั้น (สามารถใช้ด้านหลังได้)

ชื่อ-สกุล.....รหัส กลุ่ม.....ห้องสอบ.....ที่นั่งสอบ.....

ข้อ	คะแนนเต็ม	คะแนน
1	10	
2	10	
3	10	
4a	5	
4b	5	
5	10	
6	10	
รวม	60	

Solution by Assoc.Prof.Sommai Priprem, PhD.
16 February 2010

ชื่อ-สกุล.....รหัส กลุ่ม.....ห้องสอบ.....ที่นั่งสอบ.....

1. Ethylene (C_2H_4) is burned at a rate of 20 kg/h with 200 percent theoretical air during a combustion process. Assuming complete combustion and a total pressure of 100 kPa, determine (a) the air-fuel ratio and (b) the dew-point temperature of the products. (10 marks)

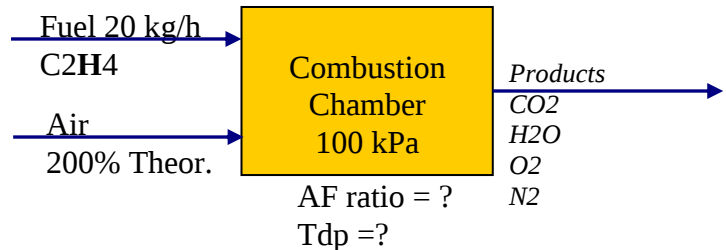
Analysis

(a) write the chemical reaction equation at 200% theoretical air

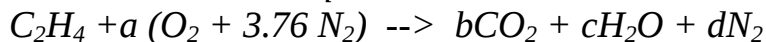
Air Fuel Ratio, $AF = m_{air}/m_{fuel}$

(b) $T_{dp} = T_{sat} @ P_v (H_2O)$

Ideal gas mixture: Dalton's Law:



(a) the chemical reaction equation at 100% theoretical air based on 1 kmol of C_2H_4



Carbon balance: $b = 2$

Hydrogen balance: $c = 4/2 = 2$

Oxygen balance: $a = (2b + c)/2 = 3$

Nitrogen balance: $d = 3.76a = 11.28$

the chemical reaction equation at 200% theoretical air



mass of air, $m_{air} = NM = (6 \times 4.76 \text{ kmol})(28.97 \text{ kg/kmol}) = 827.4 \text{ kg}$

mass of fuel, $m_{fuel} = NM = (1 \text{ kmol})[(12 \times 2 + 4 \times 1) \text{ kg/kmol}] = 28.0 \text{ kg}$

Air-Fuel ratio = $(Nm)_{air}/(Nm)_{fuel} = 827.4/28$

Air-Fuel ratio, $AF = 29.55 \text{ kg air/kg fuel}$ Answer

$m_{Fuel} = 20 \text{ kg/h}$

$m_{Air} = m_{Fuel} * AF = (20 \text{ kg/h})(19.31) = 591.0 \text{ kg/h}$ Answer

Total pressure of products = 100 kPa

Components	N	y_i	P_i
	kmol		kPa
CO ₂	2	0.0677	6.7659
H ₂ O	2	0.0677	6.7659
O ₂	3	0.1015	10.1488
N ₂	22.56	0.7632	76.3194
Sum	29.56	1.0000	100

Interpolation: Table A-5

P (kPa)	T (°C)
5	32.88
6.7659	38.11
7.5	40.29

Interpolation at $P_v = 6.7659 \text{ kPa}$ $T_{dp} = 38.11 ^\circ\text{C}$

Therefore, the dew point temperature of the products is $38.11 ^\circ\text{C}$ Answer

ชื่อ-สกุล.....รหัส.....กลุ่ม.....ห้องสอบ.....ที่นั่งสอบ.....

2) Methane (CH_4) is burned with an unknown amount of air during a combustion process. An analysis of the combustion products **on dry basis** is as follow: $\text{CO}_2 = 10.00\%$, $\text{CO} = 0.53\%$, $\text{O}_2 = 2.37\%$, $\text{N}_2 = 87.10\%$. Determine (a) the air-fuel ratio and (b) the percentage of theoretical air used during this process. (10 marks)

System: $\text{CH}_4 + \text{Air}$; Combustion

Assumption: Ideal gas

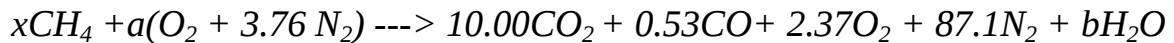
Analysis: $\%n_i = \%V_i$

$$AF = m_{\text{air}}/m_{\text{fuel}}$$

$$\% \text{theore air} = AF_{\text{actual}}/AF_{\text{theor.}} \times 100\%$$

Solution

(a) **Combustion eqn. based on 100 kmol of DRY PRODUCTS**



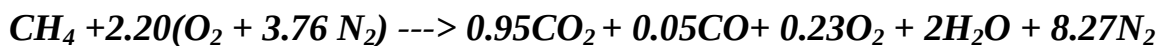
$$\text{C balance: } x = 10.00 + 0.53 = 10.53$$

$$\text{N}_2 \text{ balance: } a = 87.1/3.76 = 23.16$$

$$\text{H}_2 \text{ balance: } b = 4x/2 = 21.06$$

$$\text{O}_2 \text{ balance: } 2a = 46.33 = 2 \times 10.00 + 0.53 + 2.37 \times 2 + b = 46.33 \text{ check}$$

Divided by x to get the combustion equation based on 1 kmol of fuel

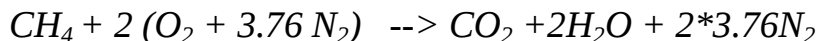


$$\text{mass of air, } m_{\text{air}} = NM = (2.20 \times 4.76 \text{ kmol})(28.97 \text{ kg/kmol}) = 303.4 \text{ kg}$$

$$\text{mass of fuel, } m_{\text{fuel}} = NM = (1.0 \text{ kmol})[(12+4) \text{ kg/kmol}] = 16.0 \text{ kg}$$

$$\begin{aligned} \text{Air-Fuel ratio} &= (Nm)_{\text{air}}/(Nm)_{\text{fuel}} = (303.4 \text{ kg})/(16 \text{ kg}) \\ &= \mathbf{18.96 \text{ kg air/kg fuel}} \quad \text{Answer} \end{aligned}$$

(b) **Theoretical Combustion**



$$\text{mass of air, } m_{\text{air}} = NM = (2.0 \times 4.76 \text{ kmol})(28.97 \text{ kg/kmol}) = 275.8 \text{ kg}$$

$$\text{mass of fuel, } m_{\text{fuel}} = NM = (1.0 \text{ kmol})[(12+4) \text{ kg/kmol}] = 16.0 \text{ kg}$$

$$\text{Theoretical Air-Fuel ratio} = (Nm)_{\text{air}}/(Nm)_{\text{fuel}} = (275.8)/(16 \text{ kg})$$

$$\text{AF theoretical} = \mathbf{17.2372 \text{ kg air/kg fuel}}$$

$$\% \text{Excess air} = [\text{AF}_{\text{actual}}/\text{AF}_{\text{theoretical}}] \times 100\%$$

$$\begin{aligned} &= \mathbf{(18.96 \text{ kg air/kg fuel}) / (17.24 \text{ kg air/kg fuel}) \times 100} \\ &= \mathbf{110.0 \%} \quad \text{Answer} \end{aligned}$$

ชื่อ-สกุล.....รหัส กลุ่ม.....ห้องสอบ.....ที่นั่งสอบ.....

3. Benzene gas (C_6H_6) at $25^\circ C$ is burned during a steady-flow combustion process with 95 percent theoretical air that enters the combustion chamber at $25^\circ C$. All the hydrogen in the fuel burns to H_2O , but part of the carbon burns to CO. If the products leave at 1000 K, determine

- (a) the mole fraction of the CO in the products and
(b) the heat transfer from the combustion chamber during this process.

(10 marks)

System: cv combustion chamber:

Combustion: $C_6H_6 + \text{Air}$

Assumptions:

- SSSF process
- $w = 0$, $\Delta KE = \Delta PE = 0$
- Air and combustion gases are ideal gas

Analysis:

- Write the combustion equation equation based on 1 kmol of C_6H_6
- Apply 1 st Law to determine Q_{cv}

$$Q_{cv} + \sum N_i \bar{h}_i = W_{cv} + \sum N_e \bar{h}_e$$

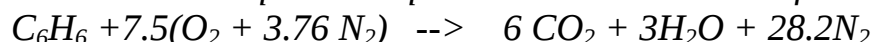
$$\sum N_i \bar{h}_i = \sum N_e \bar{h}_e$$

$$\sum N_R \{ \bar{h}_f^o + (\bar{h} - \bar{h}^o) \}_R = \sum N_P \{ \bar{h}_f^o + (\bar{h} - \bar{h}^o) \}_P$$

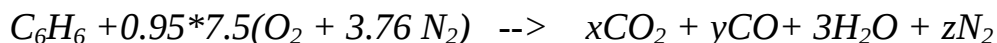
$$\because \text{reactants are at reference state } (\bar{h} - \bar{h}^o)_R = 0$$

$$\sum N_R \{ \bar{h}_f^o \}_R = \sum N_P \{ \bar{h}_f^o + (\bar{h} - \bar{h}^o) \}_P$$

Theoretical Combustion equation equation based on 1 kmol of C_6H_6



Combustion with 95% theoretical air



C balance: $x + y = 6$

O balance: $2x + y + 3 = 0.95 \cdot 7.5 \cdot 2 = 14.25$

$$2x + y = 11.25$$

$$x = 11.25 - 6 = 5.25$$

$$y = 6 - 5.25 = 0.75$$

$$z = 0.95 \cdot 7.5 \cdot 3.76 = 26.79$$

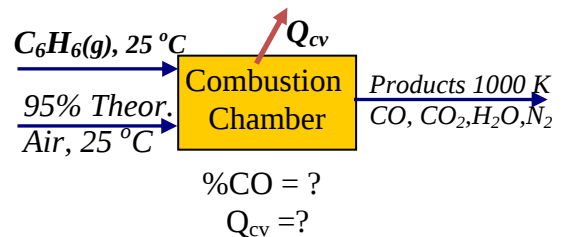
therefore the combustion equation is ($T_p = 1,000K$, so water is in vapor form)



$$\sum n \text{ in products} = 5.25 + 0.75 + 3 + 26.79 = 35.79 \text{ kmol}$$

$$\% \text{ CO in products} = (n_{CO} / \sum n) \cdot 100\% = (0.75 / 35.79) \cdot 100\%$$

$$= 2.10 \% \quad \text{Answer}$$



(b) Energy analysis of the combustion process

Reactants at 25 °C: $H_R = h_f^\circ(C_6H_6) = 82,930 \text{ kJ/kmol}$

Products at 1000 K

Components	n	h_f°	h_{1000}	h_{298}	$(h_i - h_{298})$	nh
	(Kmol)	(kJ/kmol)	(kJ/kmol)	(kJ/kmol)	(kJ/kmol)	(kJ)
CO ₂	5.25	- 393,520	42,769	9,364	33,405	-1,890,603.8
CO	0.75	- 110,530	30,335	8,669	21,666	-66,648.0
H ₂ O	3.00	- 241,820	35,882	9,904	25,978	-647,526.0
N ₂	26.79	-	30,129	8,669	21,460	574,913.4
Sum (H _p)						- 2,029,864.4

$$Q_{cv} = H_p - H_r = -2,112,794.4 \text{ kJ/kmol fuel}$$

$$M_{fuel} = 78 \text{ kg/kmol}$$

$$q_{cv} = -2,112,794.4 \text{ (kJ/kmol fuel)} / 79 \text{ (kg/kmol)}$$

$$= -27,087.1 \text{ kJ/kg}$$

the heat transfer from the combustion chamber is 27,087.1 kJ/kg fuel Answer

Solution by Assoc.Prof.Sommaipriprem, PhD.
16 February 2010

ชื่อ-สกุล.....รหัส กลุ่ม.....ห้องสอบ.....ที่นั่งสอบ.....

4a) Consider the F-18 Fighter plane specification. If the air temperature at the cruising altitude is about -70°C . Determine the maximum Mach number of this plane at this condition. (5 marks)

	Name: <u>F/A-18 Hornet</u>	Armament: 1 cannon 20 mm 2 Sidewinders 6,220 kg max payload
	Constructor: McDonnell Douglas	
	Length: 17m08	Max Speed: 1,900 km/h
	height: 4m63	Ceiling: 15,250 m
	Span: 11m44	Weight Max: 22,317 kg
	Crew: 1	Range: 3,670 km
		Engines: 2

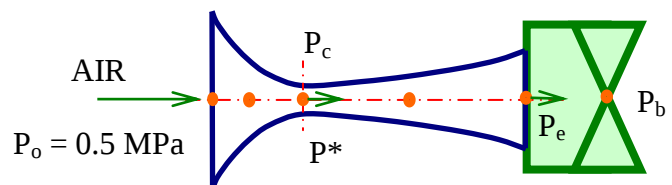
System: Air, Ideal gas

Analysis: $M = V/c$
 $c = \sqrt{kRT}$

Solution Maximum speed = 1,900 km/h
Velocity = $(1,900\text{km/h}) \cdot (1,000\text{m/km}) / (3,600\text{ s/h}) = 527.8\text{ m/s}$
Table A-1 for air: $R = 0.287\text{ kJ/kgK}$
Table A-2a at 300 K: $k = 1.4$
 $c = \sqrt{kRT} = \sqrt{(1.4)(287\text{ J/kgK})(273-70)\text{K}}$
 $= 285.6\text{ m/s}$
 $M = V/c = (527.8\text{ m/s}) / (285.6\text{ m/s}) = 1.85$

The maximum Mach number of this plane at this condition is 1.85 Answer

4b) Air enters a converging-diverging nozzle at 0.5 MPa with a negligible velocity. Assuming the flow to be isentropic, determine **the back pressure** that will result in an exit Mach number of 1.8. (5 Marks)



System: Air, Conv.-Div.Nozzle

Assumption: Ideal gas, constant sp.ht.

Isentropic flow

Solution Fluid: Air $k = 1.4$

Given $P_o = 500\text{ kPa}$

$M_e = 1.8$

Table A-34, @ $M=1.8 = P/P_o = 0.17404$

$P_B = P_e = 0.17404 \cdot P_o = (0.17404) \cdot (500\text{ kPa}) = 87.02\text{ kPa}$

The back pressure, P_B is 87.02 kPa Answer

ชื่อ-สกุล.....รหัส กลุ่ม.....ห้องสอบ.....ที่นั่งสอบ.....

5. Consider a supersonic wind tunnel as shown in the figure below. Air enters a **converging-diverging nozzle** at 4 MPa and 25°C with a low velocity. The cross-sectional area of the test section is equal to the exit area of the nozzle, which is 5 m². If it is required that the velocity of the air entering the test section is one and a half time of the speed of sound (Mach number, Ma = 1.5). **Calculate** the pressure, temperature, velocity, and mass flow rate in the test section (8 marks). **Explain why the air inside this system must be very dry.** (2 marks)

System: Air, Conv.-Div.Nozzle

Assumption: Ideal gas, constant sp.ht.

Isentropic flow

Analysis: $V_1 = 0$ then

$T_{01} = T_1$ and $P_{01} = P_1$

Isentropic flow: $P_{02} = P_{01}$, $T_{02} = T_{01}$

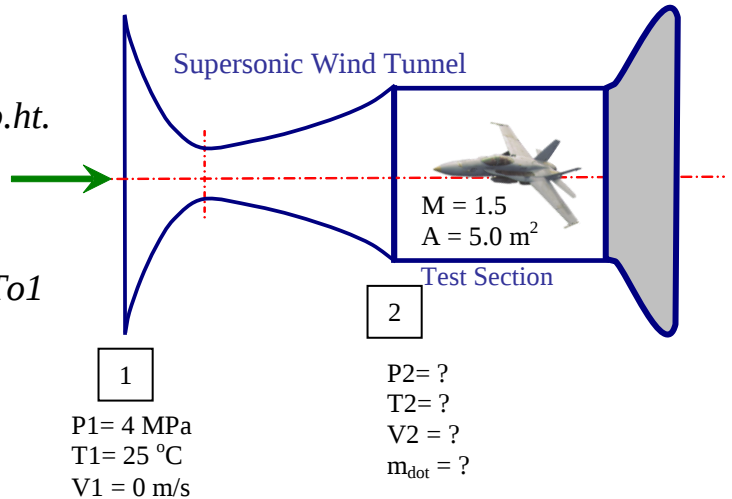
$\dot{m} = \rho A V$

$V = MC$

Solution:

$P_0 = 4 \text{ MPa} = 4000 \text{ kPa}$

$T_0 = 25^\circ\text{C} = 298 \text{ K}$



At the exit plane

Using Table A-34 for $M = 1.5$, $P/P_0 = 0.27240$, and $T/T_0 = 0.68965$

$P_2 = 0.2724 P_0 = 0.2724 * 4000 \text{ kPa} = \mathbf{1,089.6 \text{ kPa}}$ **Answer**

$T_2 = 0.68965 T_0 = 0.68965 * 298 \text{ K} = \mathbf{205.5 \text{ K}}$ **Answer**

Table A1, A2 for air at 300K; $R = 0.287 \text{ kJ/kgK}$ and $k = 1.4$

Sonic velocity, $c = \sqrt{kRT} = \sqrt{(1.4)(287 \text{ J/kgK})(205.5 \text{ K})} = 287.4 \text{ m/s}$

Velocity, $V = Mc = 1.5 * 287.4 \text{ m/s} = \mathbf{431.0 \text{ m/s}}$ **Answer**

Density, $\rho = P/RT = (1,089.6 \text{ kPa})/(0.287 \text{ kJ/kgK} * 205.5 \text{ K})$
 $= 18.47 \text{ kg/m}^3$

The exit area, $A = 5 \text{ m}^2$

**The mass flow rate of air, $\dot{m} = \rho AV = (18.47 \text{ kg/m}^3)(5 \text{ m}^2)(431.0 \text{ m/s})$
 $= \mathbf{39,813.4 \text{ kg/s}}$ **Answer****

อากาศที่ไหลในอุโมงค์ลมนี้ มีความเร็วสูงมาก (เหนือเสียง) ส่งผลให้อุณหภูมิลดต่ำลงอย่างมาก เช่น ในกรณีนี้ลดลงเป็น 205 K หรือ ประมาณเกือบ -70°C ดังนั้นหากในอากาศมีความชื้น มันจะเปลี่ยนสถานะเป็นของแข็ง (น้ำแข็ง)ทันที เกล็ดน้ำแข็งนี้แม้จะมีขนาดเล็กมากแต่มันเคลื่อนที่ด้วยความเร็วเหนือเสียง นอกจากจะรบกวนกระแสอากาศทำให้การวัดปริมาณต่างๆผิดพลาดแล้ว ยังสามารถทำความเสียหายให้อุปกรณ์ต่างๆได้อีกด้วย ดังนั้น ใน Supersonic Wind Tunnel จึงจำเป็นต้องใช้อากาศที่แห้ง โดยกำจัดความชื้นในอากาศออกก่อน

ชื่อ-สกุล.....รหัส กลุ่ม.....ห้องสอบ.....ที่นั่งสอบ.....

6. Steam entering turbine blades with a **velocity** of 900 m/s and the **angle** is 20° . The **blade velocity**, V_B is 300 m/s and the **blade velocity coefficient**, k_B is 0.7. The turbine is an **impulse turbine** ($P_{\text{flow in blade}} = \text{constant}$) and the blade is **symmetrical** (the **angle** of the entering relative velocity and the leaving relative velocity are equal). Draw the velocity diagram and calculate for the mass flow of 15 kg/s,

(a) the blade inlet angle

(b) the power out put of the turbine

(c) the blade efficiency (diagram efficiency)

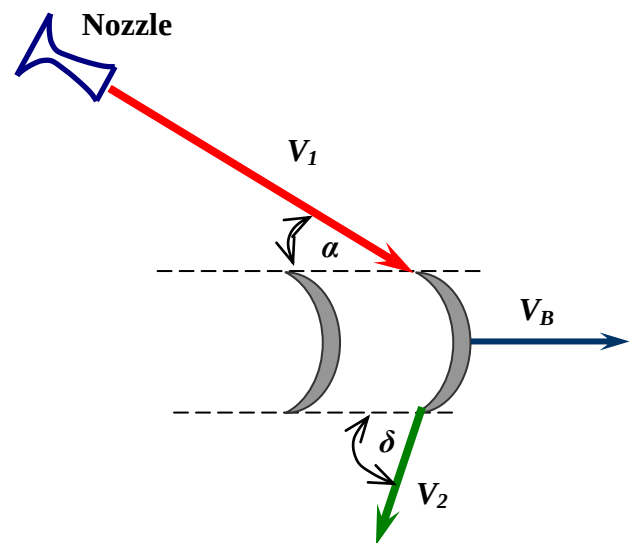
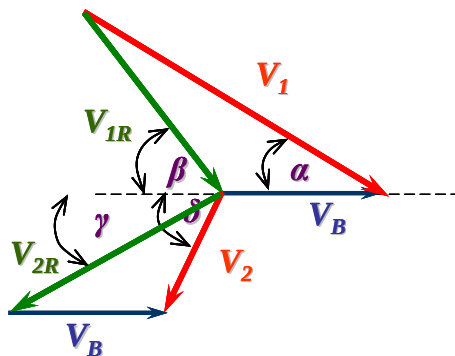
(d) the axial thrust (assume constant x-section flow area)

(10 marks)

(note: $k_B = V_{2R}/V_{1R}$)

Given:

- $V_1 = 900 \text{ m/s}$; $\alpha = 20^\circ$
- $V_B = 300 \text{ m/s}$
- $k_B = V_{2R}/V_{1R} = 0.7$



Determine: β , W , η_B , R_a

Triangle ACD: law of cosines

$$c^2 = a^2 + b^2 - 2ab \cos \alpha$$

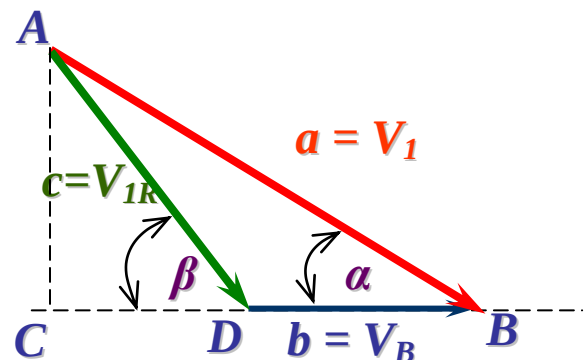
$$V_{1R} = c = 626.5 \text{ m/s}$$

Triangle ABD: law of sines

$$c/\sin \alpha = a/\sin(180^\circ - \beta) = a/\sin \beta$$

$$\sin \beta = (a/c)(\sin \alpha) = 0.491$$

the blade inlet angle, $\beta = \sin^{-1}(0.491) = 29.41^\circ$ answer(a)



Tangential Thrust; $R_t = m_{\dot{m}}(V_{1R} \cos \beta + V_{2R} \cos \gamma)$

$$k_B = V_{2R} / V_{1R} = 0.7 \rightarrow V_{2R} = 0.7V_{1R} = 0.7 \times 626.5 = 438.5 \text{ m/s}$$

symmetrical blading ($\beta = \gamma$).

$$R_t = m_{\dot{m}} (626.5 \cos 29.41 + 438.5 \cos 29.41)$$

$$R_t / m_{\dot{m}} = 927.7 \text{ N/(kg/s)}$$

the driving force on the wheel per 1 kg/s

$$R_t / m_{\dot{m}} = 927.7 \text{ N/(kg/s)}$$

the turbine power, $W_{\dot{m}} = m_{\dot{m}} V_B R_T$

$$W_{\dot{m}} = (15 \text{ kg/s})(300 \text{ m/s})(927.7 \text{ N/kg/s}) / (1000 \text{ W/kW}) = 1,474.5 \text{ kW}$$

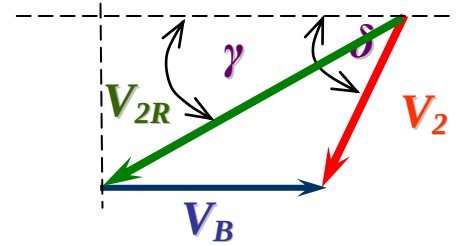
the power out put of the turbine is 1,474.5 kW answer (b)

(e) the blade efficiency, $\eta_D = w / ke_1 = W_{\dot{m}} / KE_{1\dot{m}}$

$$KE_{1\dot{m}} = m_{\dot{m}} V_1^2 / 2 = (1 \text{ kg/s})(900 \text{ m/s})^2 / (2 \times 1000 \text{ W/kW}) = 810 \text{ kW}$$

$$\eta_B = (278.3 \text{ kW}) / (810 \text{ kW}) \times 100\% = 68.7\%$$

the blade efficiency (diagram efficiency), η_B , is 68.7% answer (c)



Axial Thrust;

$$R_a = m_{\dot{m}} (V_{2R} \sin \gamma - V_{1R} \sin \beta) - (P_1 A_1 - P_2 A_2)$$

Impulse turbine $\rightarrow \Delta P$ across blade = 0, therefore, $P_1 = P_2$

Symmetry blading $\rightarrow A_1 = A_2$

$$\text{So } (P_1 A_1 - P_2 A_2) = 0$$

$$\text{then } R_a = m_{\dot{m}} (V_{2R} \sin \gamma - V_{1R} \sin \beta)$$

$$\begin{aligned} R_a &= (15 \text{ kg/s})(438.5 \sin 29.41 - 626.5 \sin 29.41) \\ &= [15 \text{ kg/s}] * [-92.3 \text{ N/(kg/s)}] = -1,384.5 \text{ N} \end{aligned}$$

The axial thrust is 1.38 kN $\uparrow$ answer (d)