

ภาควิชาวิศวกรรมเครื่องกล

คณะวิศวกรรมศาสตร์ มหาวิทยาลัยขอนแก่น

ข้อสอบปลายภาค ประจำภาคต้น ปีการศึกษา 2553

วิชา **185 231 Thermodynamics I**

วันที่ 29 กันยายน 2553

เวลา 13.00 — 16.00 น.

ผู้ออกและตรวจข้อสอบ: รศ.ดร.สมหมาย ปรีเปรม ผศ.ดร.ปริมพัฒน์ สุจ้านงโตกุล อ.ดร.อักรพล จันทรอ่อน

คำสั่ง

1. ให้เขียน ชื่อ-สกุล กลุ่ม และที่นั่งสอบ ลงในกระดาษข้อสอบทุกแผ่น
2. ข้อสอบทั้งหมดมี 5 ข้อ จำนวน 8 แผ่นรวมทั้งแผ่นนี้ ให้ทำทุกข้อ
3. มีตาราง Thermodynamics ให้
4. อนุญาตให้ใช้เครื่องคำนวณที่ไม่มีการบันทึกข้อมูลของรายวิชานี้ไว้
5. ห้ามนำเอกสารใดๆออกจากห้องสอบ
6. ให้ทำข้อสอบในแผ่นข้อสอบของข้อนั้นๆเท่านั้น (สามารถใช้ด้านหลังได้)

ชื่อ-สกุล.....รหัส..... Section.....ที่นั่งสอบ.....

ข้อ	คะแนนเต็ม	คะแนน
1	10	
2	10	
3	10	
4	10	
5	10	
รวม	50	

2. An air standard Otto engine has a compression ratio of 9.0. The state of air at the beginning of the compression process is 80 kPa and 30°C. The heat input during the heat addition process is 1,000 kJ/kg. Calculates by using constant specific heats at 900 K, determine

- (a) Write the name of the 4 processes (1 mark)
 - (b) draw the P-v and T-s diagram, (1 mark)
 - (c) the amount of heat rejected per cycle, (3 mark)
 - (d) the net work per cycle, (1 mark)
 - (e) the thermal efficiency and (1 mark)
 - (f) the mean effective pressure. (2 mark)
- การทำงานที่เป็นระบบ เรียบร้อยและสะอาด (1 mark)

Process	Process name	P-v diagram	T-s diagram
1-2	<i>Isentropic Compression</i>		
2-3	Constant Volume Heat Addition		
3-4	Isentropic Expansion		
4-1	Constant Volume Heat Rejection		

Solution

Assumption: Air Standard Otto cycle, constant sp.ht.at 900K

Given: $P_1 = 80 \text{ kPa}$, $T_1 = 30^\circ\text{C}$, $r_v = 9$; $q_H = 1,000 \text{ kJ/kg}$

Constants: Table A-1: $R = 0.287 \text{ kJ/kgK}$; Table A-2(b): $C_v = 0.834 \text{ kJ/kgK}$, $k = 1.344$

therefore: $k-1 = 0.344$; $r_v^{(k-1)} = 2.1294$ and $r_v^k = 19.1647$

Process 1-2 Isentropic Expansion $Pv^k = \text{const.}$ and $Tv^{k-1} = \text{const.}$

$$P_2 = P_1(r_v^k) = (80\text{kPa})(9.0)^{1.344} = 1,533.2 \text{ kPa}$$

$$T_2 = T_1 r_v^{(k-1)} = (303\text{K})(9.0)^{0.344} = 645.2 \text{ K}$$

Process 2-3 Constant Volume Heat Addition

$$q_H = 2q_3 = u_3 - u_2 = C_v(T_3 - T_2)$$

$$T_3 = T_2 + 2q_3/C_v = (645.2)\text{K} + (1,000\text{kJ/kg}) / (0.834\text{kJ/kgK}) = 1,844.3 \text{ K}$$

Process 3-4 Isentropic Expansion $Pv^k = \text{const.}$ and $Tv^{k-1} = \text{const.}$

$$T_4 = T_3 / r_v^{(k-1)} = (\text{K}) / (9.0)^{0.344} = 866.1 \text{ K}$$

Process 4-1 Constant Volume Heat Rejection

$$4q_1 = C_v(T_1 - T_4) = (0.834\text{kJ/kgK})(303 - 866.1)\text{K} = -469.6 \text{ kJ/kg}$$

(c) The amount of heat rejected per cycle, $q_L = |4q_1| = 469.6 \text{ kJ/kg}$ **Answer**

(d) The net work per cycle, $w_{\text{net}} = q_H - q_L = (1,000 - 469.6)\text{kJ/kg} = 530.4 \text{ kJ/kg}$ **Answer**

(e) The Thermal Efficiency, $\eta_{\text{th}} = w_{\text{net}}/q_H * 100\%$
 $= (530.4 \text{ kJ/kg}) / (1,000\text{kJ/kg}) * 100 = 53.04 \%$ **Answer**

(f) Mean effective pressure, $MEP = W_{\text{net}} / (v_1 - v_2)$

$$v_1 = RT_1/P_1 = 1.08701 \text{ m}^3/\text{kg}, \text{ therefore, } v_2 = v_1/r_v = 0.12078 \text{ m}^3/\text{kg}$$

$$MEP = (530.4 \text{ kJ/kg}) / (1.08701 - 0.12078) \text{ m}^3/\text{kg} = 548.9 \text{ kPa}$$
 Answer

3. An air standard Brayton cycle has a pressure ratio of 14. The air at the compressor inlet is at 27 °C and 100 kPa. The temperature at the turbine inlet is 1200 K.

Calculates by using constant specific heats at 900 K, Determine

(a) Write the name of the 4 processes (1 mark)

(b) draw the P-v and T-s diagram, (1 mark)

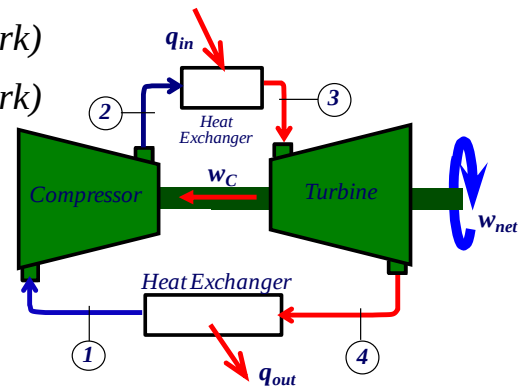
(c) the net work, (4 mark)

(d) the heat input, (2 mark)

(e) the cycle thermal efficiency. (1 mark)

การทำงานที่เป็นระบบ เรียบร้อยและสะอาด

(1 mark)



Process	Process name	P-v diagram	T-s diagram
1-2	<i>Isentropic Compression</i>		
2-3	Constant pressure heat added		
3-4	Isentropic expansion		
4-1	Constant pressure heat rejection		

Solution

Assumption: Air Standard Brayton cycle, constant sp.ht. at 900K

Given: $P_1 = 100 \text{ kPa}$, $T_1 = 27^\circ\text{C}$, $r_p = 14$; $T_3 = 1,200 \text{ K}$

Constants: Table A-1: $R = 0.287 \text{ kJ/kgK}$; Table A-2(b): $C_p = 1.121 \text{ kJ/kgK}$, $k = 1.344$

therefore: $(k-1)/k = 0.2560$; and $r_p^{(k-1)/k} = 1.9650$

Process 1-2 Isentropic Compression

$$T_2 = T_1 * r_p^{(k-1)/k} = 300\text{K} * 1.9650 = 589.5 \text{ K} \quad (\text{determine } T_2)$$

Process 3-4 Isentropic Expansion

$$T_4 = T_3 / r_p^{(k-1)/k} = 1200\text{K} / 1.9650 = 610.7 \text{ K} \quad (\text{determine } T_4)$$

To determine w_c : CV compressor :

1st Law: Open System, SSSF, $q = 0 \rightarrow q + h_1 = w + h_2$

$$w = h_2 - h_1 = C_p(T_2 - T_1) = 1.005\text{kJ/kgK}(589.5 - 300)\text{K} = -324.5 \text{ kJ/kg}$$

$$w_c = |w| = 324.5 \text{ kJ/kg}$$

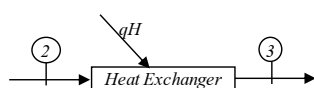
To determine w_t : CV Turbine : 1st Law: Open System, SSSF, $q = 0 \rightarrow q + h_3 = w + h_4$

$$w = h_3 - h_4 = C_p(T_3 - T_4) = 1.121\text{kJ/kgK}(1200 - 610.7)\text{K} = 660.6 \text{ kJ/kg}$$

$$w_t = |w| = 660.6 \text{ kJ/kg}$$

(c) Net work, $w_{net} = w_t - w_c = (660.6 - 324.5)\text{kJ/kg} = 336.1 \text{ kJ/kg}$ **Answer**

(d) the heat input, q_H : CV. HE + q : 1st Law: Open System, SSSF, $w = 0 \rightarrow q + h_2 = w + h_3$



$$q = h_3 - h_2 = C_p(T_3 - T_2) = 1.121\text{kJ/kgK}(1200 - 589.5)\text{K} = 684.4 \text{ kJ/kg}$$

$$\text{heat input, } q_H = |q| = 684.4 \text{ kJ/kg} \quad \text{Answer}$$

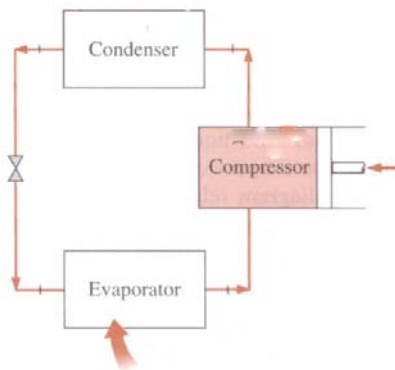
(e) The Thermal Efficiency, $\eta_{th} = w_{net}/q_H * 100\%$

$$= (336.1 \text{ kJ/kg}/684.4\text{kJ/kg})*100 = 49.11 \% \quad \text{Answer}$$

5. An ideal vapor compression refrigeration cycle that uses R-12 as its working fluid maintains a condenser at 1000 kPa and the evaporator at 4 °C.

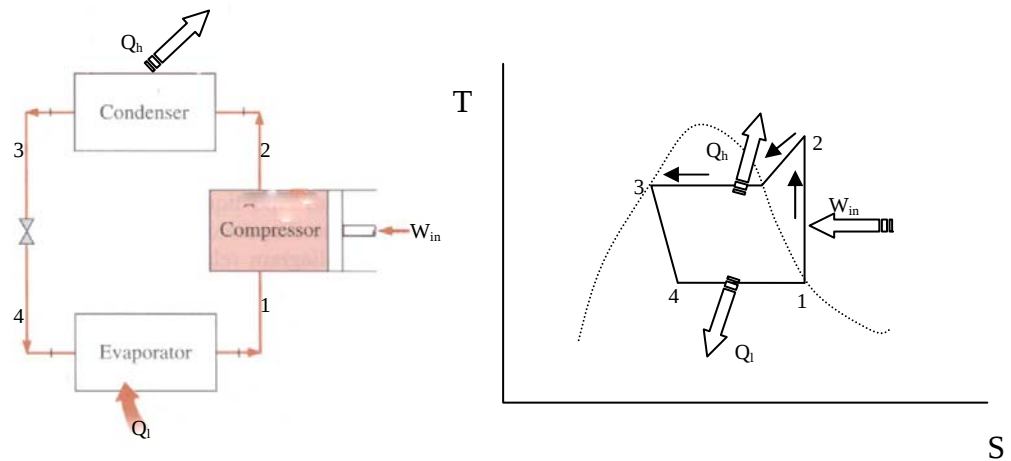
Determine:

- Draw T-s diagram of this refrigeration cycle and label all parameters: Q, W, P, T and directions of refrigerant flow with respect to the saturation line.
- The quality of the refrigerant at the evaporator inlet.
- The cooling capacity.
- The COP of this refrigerator.



Solution:

a) T-s diagram



$$T_4 = T_1 = 4\text{ }^{\circ}\text{C}$$

$$P_4 = P_1 = ?$$

$$P_3 = P_4 = 1000\text{ kPa}$$

$$T_3 = T_4 = ?$$

Step 1 – 2 is Isentropic : $s_3 = s_4$

Step 3 – 4 is Isenthalpic : $h_3 = h_4$

b) Quality of refrigerant

$$h_3 = h_{f @ 1000 \text{ kPa}} = 76.26 \quad \text{kJ / kg}$$

Table A-11

$$h_{fg @ 4^\circ\text{C}} = 149.47 \quad \text{kJ / kg}$$

$$h_{f @ 4^\circ\text{C}} = 39.76 \quad \text{kJ / kg}$$

Isenthalpic $h_3 = h_4$

$$T_4 = 4^\circ\text{C}$$

$$h_4 = h_{f @ 4^\circ\text{C}} + x(h_{fg @ 4^\circ\text{C}})$$

$$x = \frac{h_4 - h_{f @ 4^\circ\text{C}}}{h_{fg @ 4^\circ\text{C}}}$$

$$x = \frac{76.23 - 39.76}{149.47} = 0.244$$

c) The cooling capacity

$$Q_L = h_1 - h_4$$

Table A-11

$$h_1 = h_{g @ 4^\circ\text{C}} = 189.23 \quad \text{kJ / kg}$$

$$Q_L = h_1 - h_4 = 189.23 - 76.26$$

$$Q_L = 112.97 \quad \text{kJ / kg}$$

d) The COP of this refrigerator.

$$COP_R = \frac{Q_L}{W_{in}}$$

$$W_{in} = h_2 - h_1$$

Isentropic compression : $s_1 = s_2$

$$s_1 = s_{g@4^\circ C} = 0.6946 \quad kJ / kg.K$$

Table A-11

$$P_2 = 1000 kPa$$

$$s_2 = 0.6946 \quad kJ / kg.K$$

Table A-13

$$T_2 = 50^\circ C$$

$$h_2 = 210.32 \quad kJ / kg$$

$$W_{in} = h_2 - h_1 = 210.32 - 189.23$$

$$W_{in} = 21.09 \quad kJ / kg$$

$$COP_R = \frac{Q_L}{W_{in}} = \frac{112.97}{21.09}$$

$$COP_R = 5.36$$